

Transient Voltage Suppressors (TVS) for Automotive Electronic Protection

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A major challenge in automotive design is protecting electronics - such as control units, sensors, and entertainment systems - against damaging surges, voltage transients, ESD, and noise that are present on the power line. Transient voltage suppressors (TVS) are ideal solutions for automotive electronic protection and have several important parameters for these applications, including power rating, stand-off voltage, breakdown voltage, and maximum breakdown voltage. Following are definitions for these parameters.

Power rating

The power rating of a TVS is its surge-absorbing capability under specific test or application conditions. The industrial-standard test condition of 10 μ s/1000 μ s pulse form (Bellcore 1089 spec.), as shown in Figure 1. This test condition differs from the TVS ESD test condition of 8 μ s/20 μ s pulse form, as shown in Figure 2.

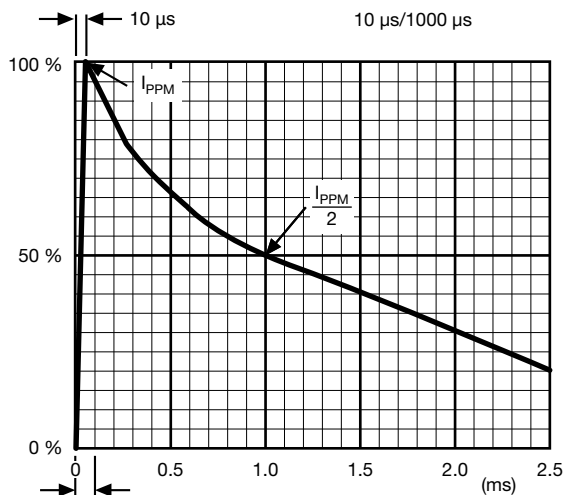


Fig. 1 - Test Waveform of TVS

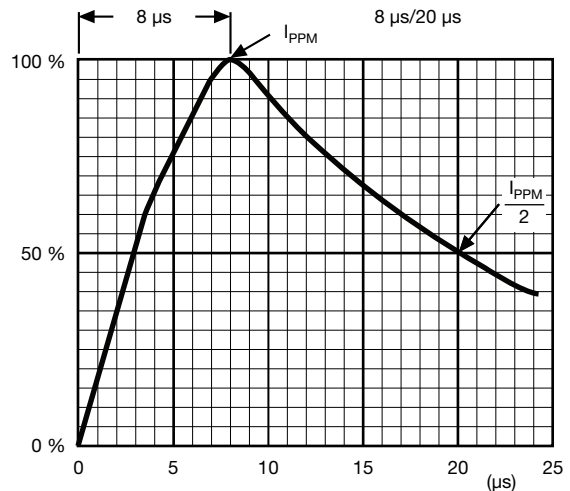


Fig. 2 - Test Waveform of TVS ESD

Breakdown Voltage (V_{BR})

The breakdown voltage is the voltage at which the device goes into avalanche breakdown, and is measured at a specified current on the datasheet.

Maximum Breakdown Voltage (V_C : Clamping Voltage)

The clamping voltage appears across the TVS at the specified peak pulse current rating. The breakdown voltage of a TVS is measured at a very low current, such as 1 mA or 10 mA, which is different from the actual avalanche voltage in application conditions. Thus, semiconductor manufactures specify the typical or maximum breakdown voltage in large current.

Stand-Off Voltage (V_{WM}): Working Stand-Off Reverse Voltage

The stand-off voltage indicates the maximum voltage of the TVS when not in breakdown, and is an important parameter of protection devices in circuits that do not operate under normal conditions. In automotive applications, some regulation of the automotive electronics is provided by "jump-start protection". This condition supplies 24 V_{DC} in 10 min to 12 V type electronics, and 36 V_{DC} in 10 min to 24 V type electronics without damage or malfunction of the circuit. Thus, the stand-off voltage is one of the key parameters in TVS for automotive electronics.

APPLICATION NOTE

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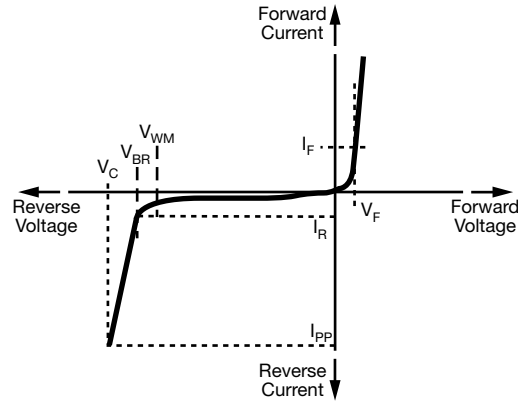


Fig. 3 - Parameters of Voltage and Current

PRIMARY PROTECTION OF THE AUTOMOTIVE POWER LINE (LOAD DUMP)

Automotive electronics, such as electronic control units, sensors, and entertainment systems, are connected to one power line. The power sources for these electronics are the battery and alternator, both of which have unstable output voltages that are subject to temperature, operating status, and other conditions. Additionally, ESD, spike noise, and several kinds of transient and surge voltages are introduced into the power and signal line from automotive systems that use solenoid loads, such as fuel injection, valve, motor, electrical, and hydrolytic controllers.

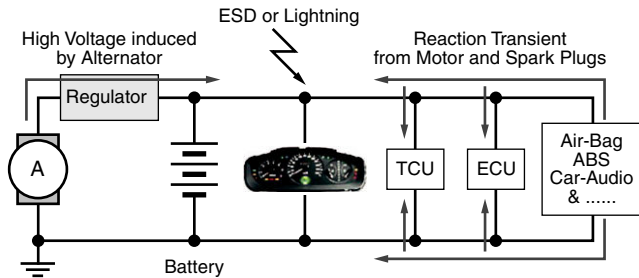
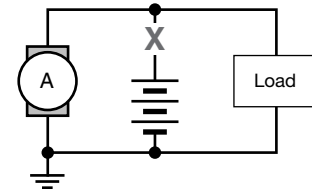


Fig. 4 - Typical Vehicle Power Bus

What is Load Dump?

The worst instances of surge voltage are generated when the battery is disconnected when the engine is in operation, and the alternator is supplying current to the power line of the vehicle. This condition is known as “load dump”, and most vehicle manufacturers and industry associations specify a maximum voltage, line impedance, and time duration for this load dump status, as shown in Figure 5.



Output Voltage of Alternator

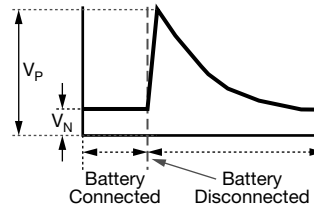


Fig. 5 - Output Voltage of Alternator in Load Dump Condition

Two well-known tests simulate this condition: the U.S.’s ISO-7637-2 pulse 5 and Japan’s JASO A-1 for 14 V powertrains and JASO D-1 for 27 V powertrains. In this section we review the application of TVS for load dump in 14 V powertrains.

Specification and Results of Load Dump Tests

The U.S.’s ISO-7637-2 pulse 5 and Japan’s JASO A-1 tests for 14 V powertrains are simulated in Table 1.

TABLE 1 - MAJOR LOAD DUMP TEST CONDITIONS FOR 14 V POWERTRAINS

| | V TOTAL (V _P) (V) | V _S (V) | V _A (V) | R _i (Ω) | TIME (ms) | CYCLE TIME |
|--------------------|-------------------------------|--------------------|--------------------|--------------------|-----------|------------|
| JASO A-1 | 70 | - | 12.0 | 0.8 | 200 | 1 |
| | 88 | - | 12.0 | 1.0 | 200 | 1 |
| ISO 7637-2 pulse 5 | 78.5 to 100.5 | 65 to 87 | 13.5 | 0.5 to 4.0 | 400 | 1 |

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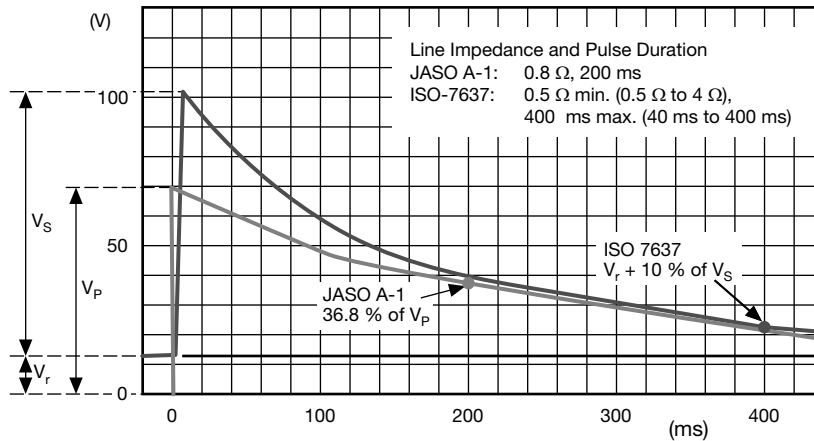


Fig. 6 - For ISO-7637-2 Test Conditions, the Standard Condition is a V_S Range of 65 V to 87 V, and R_i (Line Impedance) Range of 0.5 Ω to 4 Ω

Some vehicle manufactures apply different conditions for the load dump test based on ISO-7637-2 pulse 5. The peak clamped current of the load dump TVS will be estimated by the following equation:

Calculation for peak clamping current

$$I_{PP} = (V_{in} - V_c) / R_i$$

I_{PP} : Peak clamping current

V_{in} : Input voltage

V_c : Clamping voltage

R_i : Line impedance

Figure 6a shows the current and voltage waveforms of Vishay's SM5S24A in the ISO 7637-2 test of 87 V V_S , 13.5 V $V_{batt.}$, 0.75 Ω R_i and 400 ms pulse width.

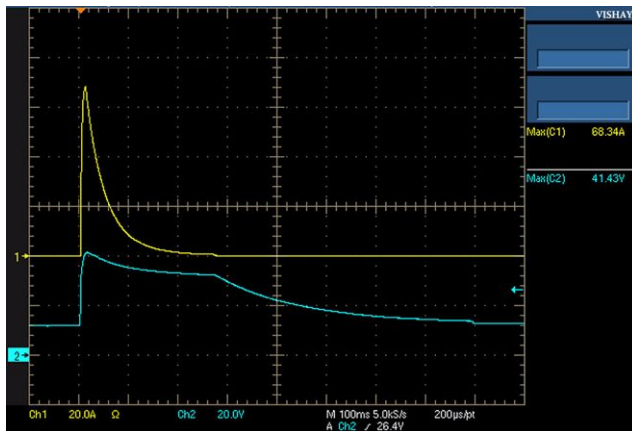


Fig. 6a - Clamped Voltage and Current of SM5A24A in ISO 7637-2 Test

Figure 6b shows the clamped voltage and current of load dummp TVF fail in the ISO 7637-2 test of 87 V V_S , 13.5 V $V_{batt.}$, 0.5 Ω R_i and 400 ms pulse width. The clamping voltage drops to near zero, and the current passed through the device is increased to the maximum allowed by the line impedance.

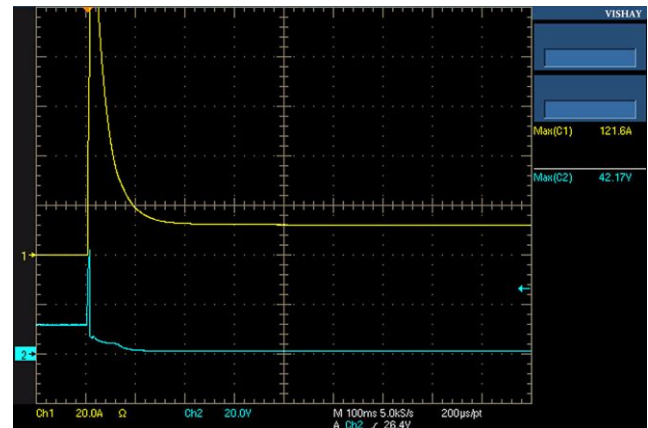


Fig. 6b - Clamped Voltage and Current of Load Dump TVS Failures in ISO7637-2 Test

Maximum clamping capability of Vishay load dump TVS of ISO 7637-2 pulse 5 test condition with 13.5 V $V_{batt.}$ and 400 ms pulse width is as Figure 6c.

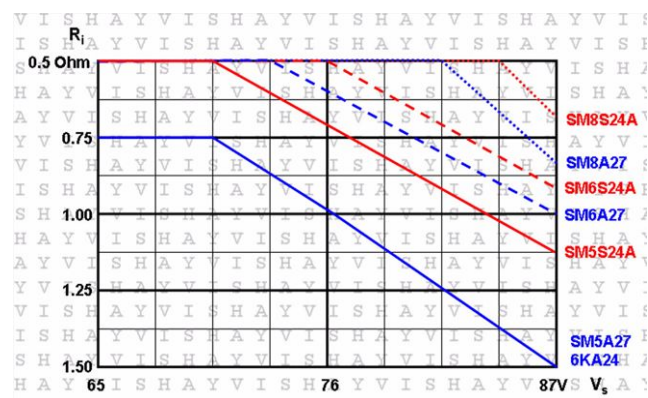


Fig. 6c - Maximum Clamping Capability of Vishay Load Dump TVS in ISO7637-2 Test

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Two Groups of Load Dump TVS

There are two kinds of load dump TVS for the primary protection of automotive electronics: EPI PAR TVS and Non-EPI PAR TVS. Both product groups have similar operating breakdown characteristics in reverse bias mode. The difference is that EPI-PAR TVSs have low forward voltage drop (V_F) characteristics in forward mode, and non-EPI PAR TVSs have relatively high V_F under the same conditions. This characteristic is important to the reverse voltage supplied to the power line. Most CMOS ICs and LSIs have very poor reverse voltage capabilities.

The gates of MOSFETs are also weak in reverse voltage, at -1 V or lower. In the reversed power input mode, the voltage of the power line is the same as the voltage of the TVS V_F . This reverse bias mode causes electronic circuit failure. The low forward voltage drop of EPI PAR TVSs is a good solution

to this problem. Another method to protect circuits from reversed power input is utilizing a polarity protection rectifier into the power line, as shown in Figure 7. A polarity protection rectifier should have sufficient forward current ratings, and forward surge and reverse voltage capabilities.

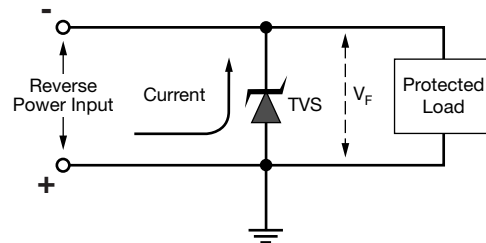


Fig. 7 - Reverse Bias Status

SECONDARY PROTECTION OF THE AUTOMOTIVE POWER LINE

The primary target of protection circuits in automotive systems is high surge voltages, but the clamped voltage is still high. Secondary protection is especially important in 24 V powertrains, such as found in trucks and vans. The main reason for this is the maximum input voltages for most

regulators and DC/DC converter ICs for automotive applications are 45 V to 60 V. For this kind of application, using secondary protection, as shown in Figure 8, is recommended.

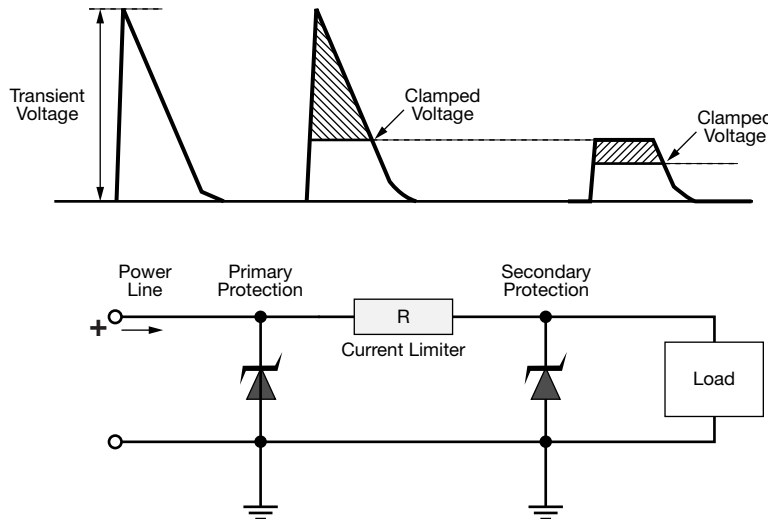


Fig. 8 - Secondary Protection Circuit

Adding resistor R onto the power line reduces the transient current, allowing smaller power-rating TVSs as the secondary protection. Current requirements for microprocessor and logic circuits in electronic units are 150 mA to 300 mA, and the minimum output voltage of a 12 V battery is 7.2 V at -18 °C, or 14.4 V for a 24 V battery under the same conditions. In a 24 V battery under the above conditions, the supply voltage at a 300 mA load is 8.4 V at $R = 20 \Omega$, and 11.4 V at $R = 10 \Omega$ at a minimum voltage of battery of 14.4 V (24 V battery voltage in -18 °C).

$$V_L = (V_{min.} / (V_{min.} / I_L)) \times ((V_{min.} / I_L) - R)$$

V_L : Voltage to load
 $V_{min.}$: Minimum input voltage
 I_L : Load current
 R : Resistor value

Power rating of R = I^2R

This supply voltage is higher than the minimum input voltages for most voltage regulators and DC/DC converter ICs.